

Improvements to the RELAP5 Turbine Model

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Outline

- ***Background***
- ***Improvements to turbine model***
- ***Test Results***
- ***Summary***

Background

- ***Energy equation for turbine volume did not include dissipation due to non-ideal turbine – cannot get correct enthalpy distribution through a series of turbine components***
- ***Turbine momentum equation used normal velocity divergence term***
- ***Turbine model requires each turbine component to be preceded by another turbine component – this requires a “dummy” turbine upstream of first active turbine***

Background (cont.)

- ***Turbine components must be numbered consecutively***
- ***Second turbine junction functions as a steam extraction junction –moisture separator option desired***
- ***User specified variable turbine efficiency, frictional torque, and moment of inertia desired***

Improvements to Turbine Model

- ***Energy equation modified to include dissipation in turbine***
- ***Momentum equation for turbine inlet junction changed from central difference to backward difference***
- ***Numbering restriction removed – this removed requirement for “dummy” turbine upstream of active turbine***

Improvements to turbine model (cont.)

- ***Removal of numbering restriction adds a geometric restriction – volume upstream or downstream of a turbine component must be singly connected in the main flow direction, i.e., only one inlet and one outlet junction on this volume – automatically satisfied if turbine component preceded by or followed by another turbine component***
- ***Moisture separator option added to turbine component***
 - ***optional separator efficiency added to turbine input***
 - ***old decks run as before, modified code assumes second junction is steam extraction junction***

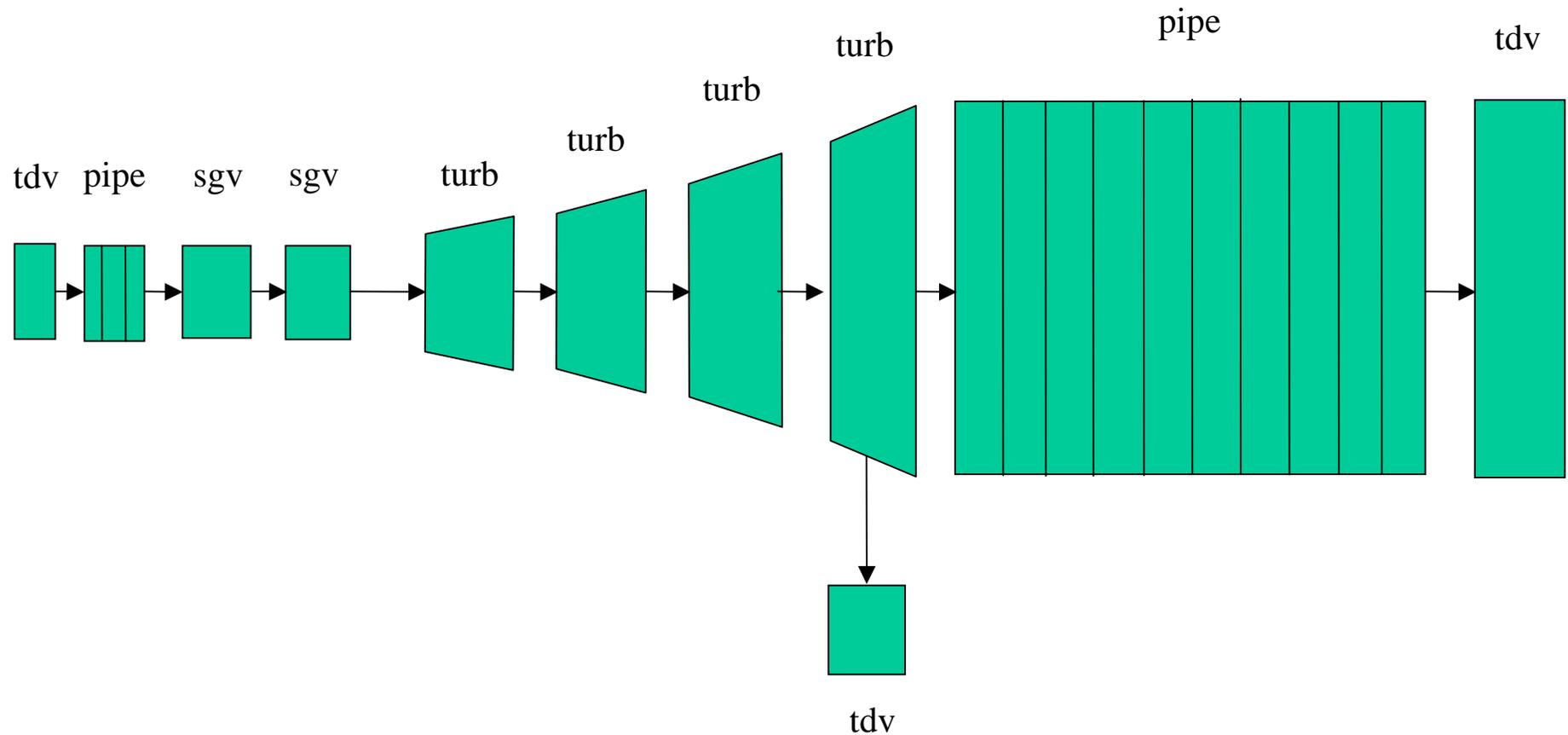
Improvements to turbine model (cont.)

- ***Turbine second junction must be connected to the “cross direction”, i.e. ‘y’ or ‘z’ faces
– old decks must be modified***

Test Case Description

- ***Existing turbine test case modified - four turbine components***
- ***“Dummy” turbine upstream of first active turbine converted to single volume***
- ***Moisture separator junction added to last turbine component for second series of test cases***
- ***Control system added to compute rate of removal of stagnation enthalpy from fluid and compare to turbine shaft power***

Test Case Schematic

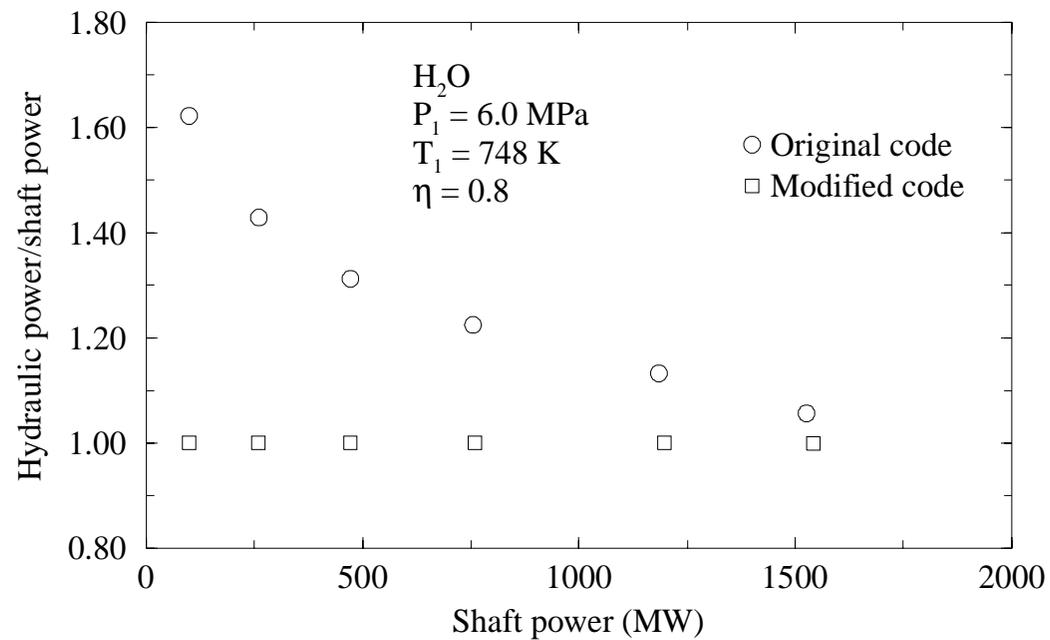


Test Case Boundary Conditions

- ***Inlet TDV pressure and temperature fixed – $6.0e+06$ Pa and 748 K***
- ***Outlet TDV pressure varied – $6.0e+06$ to $0.5e+06$ Pa***
- ***Flow rate varied from 2100 kg/sec to 3000 kg/sec***
- ***No moisture separator junction***

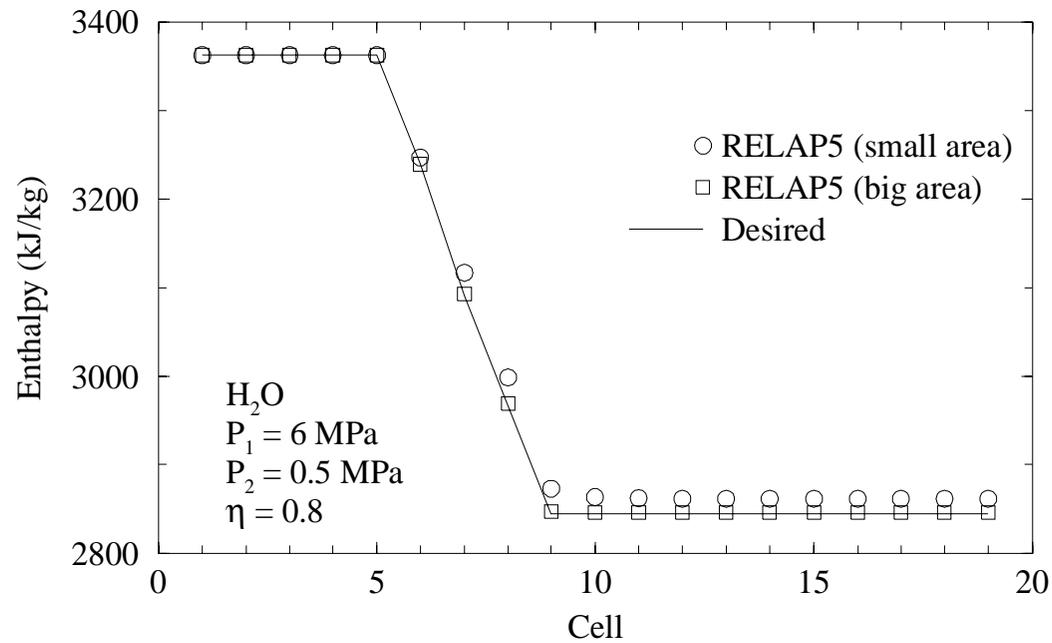
Test Results

Energy Conservation



Test Results (cont.)

Enthalpy Distribution



Test Results (cont)

- ***Two test runs with moisture separator***
- ***Reduced inlet temperature to get two-phase in last turbine component***
- ***First run with separator efficiency of 1.0e-06***
- ***Ratio of hydraulic power to shaft power 0.99848, identical to case with no separator junction***
- ***Second run with separator efficiency of 0.999***
- ***Ratio of hydraulic power to shaft power 0.99847***
- ***Flow rate of liquid out separator junction equal to amount of liquid removed by separator***

Summary

- ***Energy equation for turbine volume corrected***
- ***Modified geometric constraints for turbine components***
- ***Test results verify that turbine improvements implemented correctly and producing expected results***
- ***New user specified efficiency, frictional torque, and moment of inertia options added***